S/148/60/000/009/007/025 A161/A030

The quality of steel ...

starting oxidization with iron ore and oxygen after the formation of slag. Two heats were melted with solid charge by conventional techniques, with iron ore for oxidizing. The behaviour of nitrogen was different in the two steel types, which may be explained by the difference in the reducing period conditions. The conclusion was made that nitrogen content in ready steel did not depend on the nature of the metal charge. The steel quality was evaluated by macrostructure and mechanical properties. All ingots were solid; the development of the transcrystallization zone did not depend on the composition of the metal charge and oxidizers; the crystalline structure was determined by the tapping temperature; the metal grain size was also not affected by the nature of the charge, it was obviously determined by the final deoxidization (both steel grades were deoxidized with aluminum). The conclusion: steel melted from a liquid semi-product is the same as regards its mechanical properties as steel melted from solid metal. The mean heat time with liquid semi-product was 2 hr 05 min (or 40.7%) shorter than with solid metal in melting ShKh15 steel, and 2 hr 02 min (45%) shorter in melting "45" steel. The electric power consumption was reduced 37.1% and 35.7% respectively. General conclusions: 1) Steel melted from a liquid

Card 3/4

S/148/60/000/009/007/025 A161/A030

The quality of steel ...

semi-product is equivalent with steel melted from solid metal in the content of nonmetallic inclusions, oxygen and nitrogen and in its mechanical properties. 2) The duration of heat with liquid semi-product is nearly twice shorter, and the consumption of electric power nearly 40% lower. There are 4 figures and 3 tables.

ASSOCIATION: Moskovskiy institut stali (Moscow Steel Institute)

SUBMITTED: 20 January 1960

Card 4/4

5/148/60/000/011/002/015 A161/A030

Chernyakov, V. A.; Samarin, A. M. AUTHORS:

Desulfuration of liquid metal with siag in vacuum treatment TITLE:

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Chernaya metallurgiya,

no. 11, 1960, 32 - 35

Information is given on laboratory experiments at the Moscow Steel Institute. It is said in a brief introductory review that the slag treatment idea came from Engineer A. S. Tochinskiy (in 1925), was later developed abroad by Zhiro and Perren (Russian spelling) (Ref. 2: M. I. Aronovich and Ye. B. Kostyuchenko, took, "Development of slag treatment method abroad", 1936), and that in the USSR the Verkh-Isetskiy zavod (Verkhniy-Iset Works) desulfurized transformer steel with powder slag composed of 80 % freshly roasted lime and 20 % fluorspar during tapping (using 1.2 -1. 1 % slag mass, in weight per cent, and achieving S content reduction to 0.011 % from 0.022) transformer steel melted in an open-hearth furnace was treated with slag mixture of 83 % line, 12 % fluorspar and 5 % soda, which proved three times more effective than treatment with furnace slag during Card 1/2

S/148/60/000/011/002/015 A161/A030

Desulfuration of liquid metal

Stal', 1956, No. 1). Vacuum tapping (Ref. 5: N.F. Dubrov and A.I. Korin, The Moscow Steel Institute treatment in a ladle is now coming into use. experimented in a laboratory where vacuum treatment in a ladle was not possible; the equipment comprised a 40-kg industion vacuum furnace with a magnesite crucible. Liquid slag was prepared in a graphite crucible within an induction furnace. Slags selected in preliminary experiments were: 1) 80 % lime with 20 % fluorspar, and 2) 50 % lims and 50 % alumina. A slag mixture of lime and fluorspar was then heated to 800°C and put on the metal surface, and the lime-alumina mixture was melted and poured onto the metal. Conclusions: 1) Ten minutes treatment in vacuum with slag of lime with fluorspar reduces S content in steel 80 %; 2) same treatment with lime-alumina slag reduces S content 45 %; 3) The proper quantity of lime-alumina slag is 2 - 4 % of the weight of the metal. There are 3 tables and 5 Soviet references.

ASSOCIATION: Moskovskiy institut stali (Moscow Steel Institute)

SUBMITTED: July 5, 1960.

Card 2/2

SAMARIN, A.M.; LUKASHEVICH-DUVANOVA, Yu.T.; DIMANT, O.V.

Determination of nonmetallic inclusions in niobium and zirconium.

Determination of nonmetallic inclusions in niobium and zirconium.

Trudy Kom. anal. khim. 12:94-107 '60.

(MIRA 13:8)

(Hobium—Analysis)

(Hometallic minerals)

NIKOLAJENKO, E.; SZAMARIN, A.; BURAKOV, Sz. Die casting of castings modified by magnesium. Musz elet 15 (KEAI 9:6) no.6:10 160. (Magnesium) (Steel)

SAMARIN, A.M.; MCHEDLISHVILI, V.A.; LYUBIMOVA, G.A.

affect of the thermal treatment on the processes of anodic
solution of ball-bearing steel. Zav.lab. 26 no.9:1052-1055
solution of ball-bearing steel. Zav.lab. 26 no.9:1052-1055
(MIRA 13:9)
'60.

1. Institut metallurgii im. A.A.Baykova Akademii nauk SSSH.
(Steel--Heat treatment)
(Steel--Analysis)

s/032/60/026/011/006/035 B015/B066

Mchedlishvili, V. A., Lyubimova, G. A., and Samarin, A. M.

AUTHORS:

Method of Electrolytic Dissolution of Stainless Steel

TITLE:

PERIODICAL:

Zavodskaya laboratoriya, 1960, Vol. 26, No. 11,

pp. 1212-1219

TEXT: The methods described in publications (Refs. 1-4) for electrolytic dissolution of stainless steel and high-chromium steels for isolating carbides and nonmetallic inclusions are inappropriate. When checking the method of N. A. Saverina (Ref. 2) N. M. Popova, A. F. Platonova, and K. P. Leonova (Ref. 5) found that at high current densities a dissolution of the carbides and a considerable contamination of the anode deposits occur. The authors of the present paper checked the methods of Refs. 1 and 2 for the isolation of oxide inclusions in steels of the 1X18H9 (1Kh18N9) and 1X18H9T (1Kh18N9T) types and also noted that the anode deposits work approach to the content of the steels of the 1X18H9 (1Kh18N9T) types and also noted that the anode deposits work approach to the content of the steels of the deposits were appreciably contaminated. They further studied the electrolytic method devised by Klinger and Koch (Refs. 6,8) on an

card 1/2

Method of Electrolytic Dissolution of Stainless Steel

S/032/60/026/011/006/035 B015/B066

electrolyzer of simpler design, and determined the optimum compositions of the catholyte and the anclyte as well as the operational conditions. The most suitable current density was found to be at 0.03 - 0.05 a/cm², if a neutral anolyte with 5% KCNS + 1% sodium citrate + 0.08% As 203 and a catholyte consisting of 5% sodium citrate acidified with citric acid to give a pH = 2.5 - 3 are used in the flow-system. Under these conditions a uniform dissolution of the steel sample is attained and no by-products are formed. A good isolation of the carbide fraction is achieved. The X-ray structure analysis of the carbide deposit of the two steels mentioned above shows that they consist of (Cr, Fe)23C6 and/or carbides enriched in titanium. A chemical analysis of the cxide inclusions obtained from an anode deposit of 1Kh18N9 steel which had been treated with chlorine, shows that mainly SiO2 and Al2O3 occur which is in agreement with the results of the vacuum melting. There are 5 figures, 3 tables, and 12 references: 8 Soviet and 4 German.

ASSOCIATION: Institut metallurgii im. A. A. Baykova Akademii nauk SSSR (Institute of Metallurgy imeni A. A. Baykov of the Academy of Sciences of the USSR)

Card 2/2

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s/020/60/132/03/23/066 B014/B011

Corresponding Member Samarin .. M., Vertman, A. A., AUTHORS :

of the AS USSR

Card 1/3

Viscosity of Liquid Nickel and Its Copper Alloys

TITLE:

Doklady Akademii nauk SSSR, 1960, Vol. 132, No. 3, PERIODICAL: pp. 572-575

TEXT: By way of introduction, the authors state that there are few publications available so far on the behavior of alloys in the liquid state that give rise to solid solutions. Reference is made in this connection to a paper by F. Gaybullayev (Ref. 1), who investigated the electrical conductivity of systems Ag-Au, In-Pb, and Bi-Sb. As was found there, the form of the isotherms of electrical conductivity does not differ from the one applying to solid solutions. Reference is further made to papers by K. Hondo and H. Endo (Ref. 2), who investigated the magnetic susceptibility of bismuth alloys with antimony in the temperature range of 20-680°C. These authors showed that the change of the isothermal magnetic susceptibility in dependence of concentration proceeds in a linear manner. The authors of the article under review

Viscosity of Liquid Nickel and Its Copper Alloys

S/020/60/132/03/23/066 B014/B011

obtained a similar result for system Ni-Co (Ref. 3). Other articles (Refs. 4-6) showed the unlimited reciprocal solubility in the systems Au-Ag, Cu-Au, and Bi-Sb in the liquid state as well. The authors of the present paper studied the viscosity of system Ni-Cu in a hightemperature viscosimeter in helium atmosphere. The temperatures were measured with a Pt-PtRh thermoelement. Measurement results are shown in Table 1 and in the three diagrams (Figs. 1-3). It may be observed from Fig. 1 that the isothermal viscosity for temperatures 1500 and 1600°C proceeds in an almost linear manner. Fig. 2 is a graphic representation of the logarithm of the kinematic viscosity log v in dependence of 10-3/T. Experimental data can be described here by the relation $\log V = A/T + B$ (A, B are constant). The identity of the part played by nickel and copper atoms in the transmission of pulses may be observed from the results. With reference to an anomaly in the temperature dependence of the viscosity of nickel pointed out by D. K. Belashchenko, this anomaly is brought into connection with the desoxidizing action of the hydrogen in which measurements were made. This is said to have given rise to a reduction of solved oxygen content in nickel, which in its turn influences viscosity. The authors under-

Card 2/3

Viscosity of Liquid Nickel and Its Copper Alloys S/020/60/132/03/23/066 B014/B011

took experiments to check this assumption. Results are graphically depicted in Fig. 3. No anomaly in viscosity was detected. Finally, data concerning viscosity are given for practical purposes. Thus, nickel has a dynamic viscosity of 0.0410 poise at 1500°C. There are 3 figures, 1 table, and 13 references, 8 of which are Soviet.

ASSOCIATION:

Institut metallurgii Akademii nauk SSSR (Institute of Metallurgy of the Academy of Sciences, USSR)

SUBMITTED:

February 5, 1960

Card 3/3

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WERTMAN, A.A.; SAMARIN, A.M.

Magnetic susceptibility of nickel, cobalt, and iron at high no.2: temperatures in the liquid state. Dokl.AN SSSR 134 no.2: (MIRA 13:9) 326-329 S '60.

1. Institut metallurgii im. A.A. Baykova Akademii nauk SSSR.
2. Chlen-korrespondent AN SSSR (for Samarin). (Nickel--Magnetic properties) (Cobalt--Magnetic properties) (Iron--Magnetic properties) (Iron--Magnetic properties) (Iron--Magnetic properties)
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5/020/60/134/003/018/020 B004/B067

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Vertman, A. A., and Samarin, A. M., Corresponding Member

AUTHORS:

of the AS USSR

TITLE:

The State of Carbon in Liquid Cast Iron

PERIODICAL:

Doklady Akademii nauk SSSR, 1960, Vol. 134, No. 3,

pp. 629-631

TEXT: For determining the configuration of carbon in cast iron the authors centrifuged samples of liquid cast iron. The number of revolutions of the centrifuge was 1700-1900/min, acceleration was 320 g, and the duration of experiments was 1230-1275 min. The temperature was approximately 30-50°C above the melting point, and was kept constant at ±5°C by means of a Pt-PtRh thermocouple and an 300 -09 (EPP-09) electronic potentiometer. After the samples had been centrifuged, they were quenched in water and analyzed. As is shown by table 1, the centrifugal force causes an irregular distribution of carbon in the sample. Those parts of the sample which were nearer the rotational axis were enriched with C. From the angular velocity, the molecular weight of C and Fe, the Card 1/2

The State of Carbon in Liquid Cast Iron

S/020/60/134/003/018/020 B004/B067

difference between their densities, the initial concentration, the distance from the rotational axis, and from the temperature, the authors calculated the number of carbon particles in the liquid cast iron to be 2.5·10⁷, the volume of the carbon colonies to be approximately 50.10⁻¹⁸ cm³, and the particle diameter to be of the order of 10⁻⁶ cm, which corresponds to a colloidal, disperse system. They concluded therefrom that cast iron is a microheterogeneous system which is not in equilibrium, consisting of carbon-saturated iron and of carbon-saturated colonies. The authors mention papers by K. P. Bunin (Ref. 1), S. T. Konobeyevskiy (Ref. 3), and D. P. Ivanov (Ref. 2). There are 1 table and 8 Soviet references.

ASSOCIATION: Institut metallurgii im. A. A. Baykova Akademii nauk SSSR

(Institute of Metallurgy imeni A. A. Baykov of the Academy

of Sciences USSR)

SUBMITTED:

May 20, 1960

Card 2/2

SAMARIN, A.M., otv. red.; ZOLOTOV, P.F., red. izd-va; KASHINA, P.S., tekhn. red.; SHEVCHENKO, G.N., tekhn. red.

[Ingots and the properties of steel] Slitok i svoistva stali; trudy. Moskva, Izd-vo Akad.nauk SSSR, 1961. 177 p. (MIRA 15:1)

1. Konferentsiya po fiziko-khimicheskim osnovam proizvodstva stali. 5th, Moscow, 1959. 2. Chlen-korrespondent AN SSSR (for Samarin). (Steel ingots)

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"APPROVED FOR RELEASE: 08/25/2000

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87 New [Developments] in the Theory (Cont.) COVERAGE: The collection contains papers reviewing the development of openhearth steelmaking theory and practice. The papers, written by staff members of schools of higher education, scientific research institutes, and main laboratories of metallurgical plants, were presented and discussed at the Scientific Conference of Schools of Higher Education. The following topics are considered: the kinetics and mechanism of carbon oxidation; the process of slag formation in open-hearth furnaces using in the charge either ore-lime briquets or composite flux (the product of calcining the mixture of lime with beauxite); the behavior of hydrogen in the open-hearth bath; metal desulfurization processes; the control of the open-hearth thermal melting regime and its automation; heat-engineering problems in large-capacity furnaces; serodynamic properties of fuel gases and their flow in the furnace combustion chamber; and the improvement of high-alloy steel quality through the utilization of vacuum and natural gases. The following persons took part in the discussion of the papers at the Conference: S.I. Filippov, part in the discussion of the papers at the Conference: S.I. Filippov, V.A. Kudrin, M.A. Glinkov, B.P. Nam, V.I. Yavoyskiy, G.N. Oyks and Ye. V. Chelishchev (Moscov Steel Institute); Ye. A. Kazachkov and A. S. Kharitonov (Zhdanov Metallurgical Institute); N.S. Mikhaylets(Institute of Chemical Metallurgy of the Siberian Branch of the Academy of Sciences USSR); A.I. Stroganov and D. Ya. Povolotskiy (Chelyabinsk Polytechnic Institute); P.V. Umrikhin (Ural Polytechnic Institute); I.I. Fomin (the Moscow "Serp i molot" Metallurgical Plant); V.A. Fuklev (Central Asian Polytechnic Institute) Card 2/14

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TABLE OF CONTEN	rs:		5		
Foreword					
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	politekhnicheskiy Desiliconizing Pi	ent, Candidate of Teck institut - Central A g Iron by Oxygen in a	sia Polytechnic	Institute].	-00	
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Physicochemical Bases of (Cont.)		
Dynamics of Processes in the Converter Molten Metal	227	
Blancia A M Samarin, and A. Ye.		
Levenets, N.P., V.M. Pobegaylo, A.M. Samarin, and A.Ye. Khlebnikov. Laboratory Experiments in Blowing Naturally	237	
Alloyed Pig Irons [Correct title in the text: Oxidation of Chromium and Phosphorus in Oxygen Top-Blowing of Metal]		
Sobakin, M.P., and Ya.D., Verbitskiy, Study by Modeling of the Molten-Metal Hydrodynamics in a Converter During Decarburiza-	245	
[Senior Engineer V. N. Shashkov and Foreman M. Ye. Novikov participated in the research work.]		
Kvitko, M.P. Processing of Pig Iron With a High Manganese Content (4%-8%) in a Converter With the Use of the Oxygen [Blast]	256	
Card 10/16		:

Ph	ysicochemical Bases of (Cont.) SOV/5411	1
	lykov, S.T. Using Lime-Iron-Ore Briquettes for Processing Pigon in a Converter With Oxygen [Blast]	319
	PART III. NONMETALLIC INCLUSIONS AND THE PROPERTIES OF STEEL	
P M	opel', S.I., and G.F. Konovalov. Removing High-Temperature elting Inclusions From Rimmed Steel	325
. V . D	olkov, S. Ye., and A.M. Samarin. Effect of Deoxidation on the esulfurization of Steel	331
70	Sutakov, D.K. Effect of Hydrogen on the Separation of Sulfur in need to be compared to the Cast Steel	337
F	costovtsev, S. T., D. I. Turkenich, V. I. Baptizmanskiy, and K. S. Prosvirnin. Nonmetallic Oxide Inclusions in Rail Steel Made in a	344
	Converter Card 12 /16	

				10	3.1
F	hysicochemical Bases of (Cont.)		SOV/5411		
r K	Carasev, V.P., and P.Ya. Ageyev.	. Feasible Ways of tal		432	
	PART IV THE A	APPLICATION OF VACU S CONTENT IN STEEL	UM AND		
	humilov, M.A., P.V. Gel'd, and pecific Features of the Process of	F.A. Sidorenko. Some f Ferrosilicon Disintegr	ation	445	
	Gel'd, P.V., and R.A. Ryabov. Fermeability of Steel to Hydrogen		•	457	
. 1	Novik, L.M., A.M. Samarin, M.F. and D.P. Ul'yanov. Improving the Bessemer-Converter Steel by Appl			461	
	Oyks, G.N., V.I. Danilin, I.I. An	nsheles, G. A. Sokolov,	and		
	Card 14/16		* .		
,					

LOMONOSOV, Mikhail Vasil'yevich; TOPCHIYEV, A.V., akad., red.; FETROVSKIY,

I.G., akad., red.; ANDREYEV, P.N., akad., red.; BYKOV, K.M., akad., red.;

KAZANSKIY, V.A., akad., red.; SHMIDT, O.Yu., akad., red.; SHCHERBAKOV,

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TOYANTS, Kh.S., red.; SAMARIN, A.M., red.; LEBEDEV, D.M., prof., red.;

FIGUROVSKIY, N.A., prof., red.; KUZNETSOV, I.V., kand. filos. nauk, red.;

BERKOVICH, D.M., red., izd-va; NOVICHKOVA, N.D., tekhn. red.; KASHINA,

P.Ye., tekhn. red.

[Selected works in chemistry and physics] Izbrannye trudy po khimii i fizike. Red.A.V.Topchieva. Stat'ia N.A.Figurovskogo. Primechaniia G.A.Andreevoi, O.A.Lezhnevoi i N.A.Figurovskogo. Moskva, Izd-vo Akad. nauk SSSR, 1961. 560 p. (MIRA 14:11)

1. Chlen-korrespondent AN SSSR (for Delone, Koshtoyants, Samarin).

(Lomonosov, Mikhail Vasil'evich, 1711-1765)

(Chemistry) (Physics)

s/137/62/000/004/006/201 A006/A101

AUTHORS:

Averin, V. V., Samarin, A. M.

TITLE:

On the complex deoxidation of steel and alloys

PERIODICAL:

Referativnyy zhurnal, Metallurgiya, no. 4, 1962, 15, abstract 4A76 (V sb. "Fiz.-khim. osnovy proiz-va stali", Moscow, AN SSSR, 1961,

The authors analyze thermodynamical conditions of O dissolving in alloys in the presence of some deoxidizing elements, having a greater chemical affinity to 0 than the base metal. On the basis of experimental and literature data, a graph is plotted and analyzed; it shows the relationship between the strength of the oxide of the given deoxidizing element, evaluated from the difference in the partial pressure of the given oxide and liquid FeO, and concentration ratio N_{Fe}/N_{Me} in the alloy corresponding to the appearance of a pure deoxidizing oxide in an equilibrium with the alloy. The solubility of 0 in the Fedizing oxide in an equilibrium with the alloy. Cr-Si system is analyzed. In low-chromium alloys Si promotes a fuller elimination of 0 as compared with Fe-Si alloys. At a content of Si > 1% the introduc-

Card 1/2

S/137/62/000/004/006/201 A006/A101

On the complex deoxidation of steel and alloys

tion of Cr into the metal can not reduce the solubility of 0 in the alloys, since the affinity to 0 of these alloys is greater than that of Cr. The authors discuss the joint effect of Mn and Si, Mn and Al, on 0 solubility in Fe. A diagram is plotted showing the deoxidation of Fe-Si alloys with Al, Ti, V, Mn, Cr. On the basis of an analysis of literature data, the cause was revealed of a sharper decrease of 0 concentration under the effect of complex deoxidizers as compared to deoxidation of steel with plain deoxidizers.

B. Linchevskiy

[Abstracter's note: Complete translation]

Card 2/2

36421 s/137/62/000/003/005/191 A006/A101

Glinenyy, Ya., Averin, V. V., Samarin, A. M.

AUTHORS:

The effect of aluminum and titanium on oxygen solubility in an iron-

TITLE:

chrome alloy (18% Cr) .

PERIODICAL: Referativnyy zhurnal, Metallurgiya, no. 3, 1962, 10, abstract 3A60 (V sb. "Fiz-khim. osnovy proiz-va stali", Moscow, AN SSSR, 1961,

27-32)

Tests were run with electrolytic Fe, Cr, Al and sponge Ti. Heats. with Al were carried out in chemically pure corundum crucibles, and with Ti in zircon-crucibles. Samples were drawn-off into quartz tubes. The O content was determined by the method of vacuum melting, the Al content by the calorimetric or weight method, and the Ti content by the calorimetric method. The effect of Al and Ti on the O solubility in a Fe-Cr alloy (18% Cr) at 1,600 C was studied by establishing the equilibrium in the following system: metal-oxide phase - ${
m H_2-H_20}$ gas mixture with a given oxidizing potential. The authors evaluated the deoxidizing capacity of the deoxidizing elements in the alloy investigated, which corresponds to the difference in the partial energy values of 0 dissolving in

Card 1/2

S/137/62/000/003/005/191 A006/A101

The effect of aluminum ...

the initial alloy and the deoxidizing element. Al and Ti are effective deoxidizers for the alloy investigated; Si and Mn reduce the solubility of O to a considerably lower degree. Mn, in spite of its low deoxidizing capacity, reduces the content of O dissolved in the alloy investigated; this should be taken into account when replacing Ni by Mn in the given steel grades. The joint effect of Si and Ti at low concentration of the latter, causes additional decrease of the O content as compared with an alloy that was deoxidized with Ti only.

T. Kolesnikova

[Abstracter's note: Complete translation]

Card 2/2

S/137/62/000/005/002/150 A006/A101

AUTHORS:

Wang Ching-t'ang, Karasev, R. A., Samarin, A. M.

TITLE:

The effect of impurities on surface tension of pure iron

PERIODICAL:

Referativnyy zhurnal, Metallurgiya, no. 5, 1962, 8, abstract 5A47 (V sb. "Fiz.-khim. osnovy proiz-va stali", Moscow, AN SSSR, 1961,

106-111)

METERS OF THE PROPERTY OF THE

TEXT: The authors employed the method of taking photographs of a lying drop on a processed alumina backing at steel founding temperatures in purified He atmosphere to investigate $\delta_{\rm Fe}$, containing (in %): 0 0.001, C 0.001 - 0.002, S 0.002, N < 0.002, Cu and Ni - traces; and the effect upon $\delta_{\rm Fe}$ of C and 0. $\delta_{\rm Fe}$ at 1,550°C is 1,865 dyne/cm. Temperature coefficient $\delta_{\rm Fe}$ d δ /dt = -0.49 dyne/cm. degree. At 1,550°C C has no particular effect on $\delta_{\rm Fe}$. With a higher C content, raised from 0.002 to 4.15%, δ decreases from 1,865 to 1,788 dyne/cm. With an 0 content, increased from 0.001 to 0.184%, δ decreases from 1,865 to 1,056 dyne/cm. Maximum 0 adsorption is 23.4 · 10⁻¹⁰ mole/cm² at an 0 content of about 0.05%. The hypothesis is advanced, that there is a mixture of FeO and 0 ions in the surface layer, FeO being prevalent.

[Abstracter's note: Complete translation]

Card 1/1

18.3200

S/137/61/000/011/026/123 A060/A101

AUTHORS:

Samarin, A.M., Potrusayev, A.P.

TITLE:

Change in the metal composition under oxygen blow-through

PERIODICAL:

Referativnyy zhurnal. Metallurgiya, no. 11, 1961, 47, abstract 11V269 (V sb. "Novoye v teorii i praktike proiz-va martenovsk.stali", Moscow, Metallurgizdat, 1961, 379-387, Discuss. 428 - 439)

TEXT: The metal was blown-through in high-frequency furnaces with 10 and 40 kg capacity, and in an experimental 350 kg converter with basic fettling. In the course of the first 5 minutes the Si is oxidized down to traces, Mn by 80%. The oxidation rate of the carbon content at constant 02 feed rate is not uniform. At the beginning of the blow-through it constitutes 0.2-0.3% C/min and as the blowing continues it grows to 0.25-0.45% carbon/min, and at the end of the blow-through a drop in the decarbonization rate down to 0.1-0.3% C/min is observed. The effect of 02 feed rate and the distance between the tuyere and the vat surface upon the sequence and oxidation rates of C content and P content at the end of the blow through was studied in the 40 kg furnace. The rate of 02 supply varied between 100 and 150 liters/min, and the tuyere distance - between 25 and 40 mm. Card 1/2

32597 S/137/61/000/011/026/123 A060/A101

Change in the metal composition ...

As the tuyere distance is increased and the 0_2 supply rate is decreased, the V_C is decreased. At an oxygen expenditure of 150 liters per minute and additions of ore it was managed to finish the dephosphorization during the time of C oxidation. A reduction in the 0_2 expenditure or an increase of the distance between the tuyere and the metal at the end of the decarbonization process leads to raising of the content of iron oxides in the slag, and the V_C is decreased, while the V_P is somewhat increased. After the loading of 50% of the lime and ore, the vat was blown through with 0_2 . After 3 - 6 min of the blow-through the P was oxidized by 93 - 94%, C by 14.6 - 33.5%, S by 22.6 - 28%. It was established that as the lump dimensions of the lime are increased, the P content in the metal increases.

Yu. Nechkin

[Abstracter's note: Complete translation]

Card 2/2

POLYAKOV, A.Yu.; SAMARIN, A.M.; SYUY TSZEN-TSZE [Hsu TSeng-chi]

Investigating the activity of components of liquid binary alloys in the system iron - silicon. Izv. vys. ucheb. zav.; chern. met. no. 1:12-20 '61. (MIRA 14:2)

1. Institut metallurgii AN SSSR i Moskovskiy institut stali. (Iron-silicon alloys) (Activity coefficients)

VAN TSZIN-TAN [Wang Ching-t'ang] (bonkva); Chassev, R.A. (Moskva); Samanur,

A.W. (Moskva); Samanur, A.G. (Moskva)

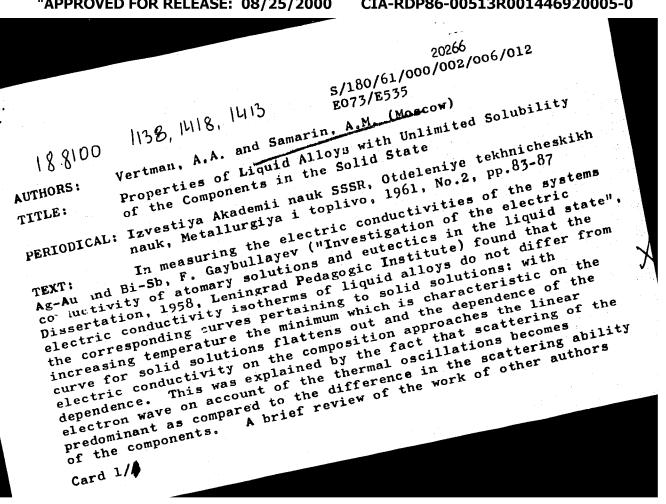
Surface tension of modten iron - sulfur - carbon, iron - ranganese - sulfur, iron - manganese - carbon. Izv. AN SSSR. Otd. tekin. nauk.

Met. i topl. no.1:15-19 Ja-F'61.

(Surface tension)

(Liquid retals)

(Liquid retals)



CIA-RDP86-00513R001446920005-0" APPROVED FOR RELEASE: 08/25/2000

Properties of Liquid Alloys ...

S/180/61/000/002/006/012 E073/E535

shows that so far only relatively low melting point systems were studied and, therefore, it was interesting to supplement the knowledge on the properties of liquid alloys of systems with unlimited solubility of the components in the solid state by studying alloys with high melting point components and, therefore, electric conductivity were measured by means of equipment described in an earlier paper (Ref.7) in a helium atmosphere. The temperature was measured by a platinum-platinum rhodium thermocouple placed The alloys were prepared by smelting The measured viscosity values are directly under the crucible. under a vacuum of 10⁻² mm Hg. under a vacuum or 10 mm ng. The measured viscosity values are plotted in Fig.1a for Ni-Cu alloys and in Fig.1b for Ni-Co alloys in terms of $v \cdot 10^2$ centistokes vs. wt.% (Cu,Co). The values given in terms of $v \cdot 10^2$ centistokes vs. wt.% (Cu,Co). were measured at the following temperatures: 1 - 1500°C, 2 - 1600°C, 3 - 1525°C, 4 - extrapolated values. The temperature dependence of the viscosity of the investigated alloys was slight. experimental values obtained on the dependence of the logarithm of the kinematic viscosity, lg y, of Ni and Cu on the inverse temperature are in good agreement with an equation of the type

Card 2/

20266 S/180/61/000/002/006/012 E073/E535

Properties of Liquid Alloys ...

 $v = K \exp \frac{E}{RT}$, $\log v = \frac{A}{T} + B$

where A, B and K are constants, E is the activation energy for viscous flow. The measured values of the electric conductivity viscous flow. The measured values of the electric conductivity are given in Fig. 3a for Ni-Cu alloys, in Fig. 3a for Ni-Co alloys, are given in Fig. 3a for Ni-Cu alloys, in Fig. 3a for Ni-Co alloys, or x 10 ohm 1, cm 1 vs. wt.% of Cu and Co, respectively. The measured values 1 were obtained for 1300°C, 2 - 1500°C, 3 -1600°C. The results are similar to those characteristic for solid solutions. However, in solid solutions the conductivity is determined basically by the differing ability of the atoms of each type to scatter electron waves, whilst in the liquid state the conductivity is mainly determined by the scattering caused by thermal oscillations. The difference in the electron structure of the atoms manifests itself also in the measured values of the magnetic properties of Fig. 4 shows the isotherm of the susceptibility, xo, in relative units, of liquid Ni-Co alloys. The experiments were carried out in a test-rig with electromagnetic scales inside an argon atmosphere using a field of 4000 Oe. The weight of the specimens did not exceed 2 g, the weighing accuracy was + 0.1 mg.

Card 3/

Properties of Liquid Alloys ...

S/180/61/000/002/006/012 E073/E535

The same figure also contains values of the average magnetic moment of the nucleus determined by the average number of vacancies in the inner electron shell of the atoms in Ni-Co system alloys (data quoted from the work of Bozorth). The measurements were made at 1600°C. Calculated values of the concentration dependence of the changes in the free energy of viscous flow in liquid Ni-Cu alloys at 1500°C (1) and Ni-Co 1525°C (2) are plotted in Fig.5. In both cases there are slight negative deviations attributed to the difference in the electron structure and to s-d-interaction. This result confirms the results obtained by O. A. Yesin and his team (Ref.10) in investigating liquid Ni-Cu alloys by the e.m.f. method. There are 5 figures, 5 tables and 10 references: 3 Soviet and 7 non-Soviet.

SUBMITTED: August 23, 1960

Card 4/#

"APPROVED FOR RELEASE: 08/25/2000 CIA-RDP86-00513R001446920005-0

SYUY TSZEM-TSZI [Heü Tsêng-ohi] (Moskva); POLYAKOV, A. Yu. (Moskva);

SAMARIN, A.M. (Moskva)

Oxygen solubility in liquid iron-silicon alloys at atmospheric pressure and in vacuum. Izv. AN. SSSR. Otd. tekh. nauk. Met. i topl. no.2:115-118 Mr-Ap '61'. (MIRA 14:4)

(Iron-silicon alloys—Oxgen.content)

S/180/61/000/003/001/012 18.3200 E111/E135

Okorokov, G.N., Polyakov, A.Yu., and Samarin, A.M. AUTHORS:

(Moscow)

Removal of oxygen in arc vacuum remelting of special TITLE:

steels

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh

nauk, Metallurgiya i toplivo, 1961, No.3, pp. 3-9

Vacuum arc remelting is now widely used for special steels and its efficacy has been established by the present authors (Ref. 3: Izv. AN SSSR, OTN, 1958, No. 5) and W.W. Dyrkacz (Ref.1: Iron Age, 1955, v. 176, No.7, and Ref.2: J. Metals, 1957, v. 9, December). The authors (Ref. 8; Filial VINITI AN SSSR, Peredovoy proizvodstvennyy i nauchno-tekhnicheskiy opyt, 1959, No. M-59-270/6) and others have studied technological and theoretical aspects of the process, but sufficient attention has not been given to the way in which it eliminates exygen and oxide non-metallic inclusions. Indications (Ref. 8) are that the more favourable vacuum conditions for reaction of metallic oxides are not due to the carbon. On the basis of results of vacuum arc Card 1/

建筑的建设的设计。 1945年代 1955年代 1955年代 1955年代 1955年代 1955年

22973 S/180/61/000/003/001/012 E111/E135

Removal of oxygen in arc vacuum remelting of special steels remelting of low-carbon iron initially deoxidized with various deoxidizers or initially not deoxidized, it was proposed that oxygen in the form of stable non-metallic inclusion could be removed without participation of the carbon (Ref. 8). To check these results the experiments have been repeated. Ingots from a 12-kg open induction furnace were forged to 40-45 mm diameter rods and two electrodes from each ingot were prepared. These were remelted in an arc vacuum furnace with a 75-mm diameter mould, one of each pair in vacuum (10-2 to 10-3 mm Hg) and the others in still argon at 760 mm Hg; silicon, manganese and aluminium were used for deoxidation. Both procedures were effective in removing oxygen, vacuum giving the better results (up to 89% removal). The amount removed was always greatly in excess of the decrease in carbon. To study the relation between the amount of CO evolved and the change in carbon and oxygen content through vacuum arc remelting, the composition and quantity of gas evolved in the remelting of deoxidized (silicon, aluminium, manganese) and not deoxidized low-carbon iron was investigated. Pressure change (in the range Card 2/6

S/180/61/000/003/001/012 E111/E135

Removal of oxygen in arc vacuum remelting of special steels 10^{-3} to 5 x 10^{-2} mm Hg) in a constant volume was used to measure the quantity of gas evolved in one minute (assumed independent of pressure). The melting current was 1200 amp, the voltage 21-23 V. The rate of melting of deoxidized iron was 450-400 and of undeoxidized 400-315 g/min. At low gas evolutions all the gas was assumed to be CO. The results are shown in Table 2. In the deoxidized metal the product of dissolved oxygen and carbon changes little on vacuum remelting and remains well above even the atmospheric-pressure equilibrium value. From the melting conditions it appears that flotation (i.e. effects leading to the concentrations of inclusions at or near the surface) must be an important factor. In manganese-deoxidized metal, where the carbon reaction is favoured by inclusions of x FeO. y MmO or MmO on which CO bubbles can nucleate, both factors are important; in undeoxidized metal the carbon reaction is decisive. With undeoxidized metal the boil produced by vacuum remelting makes this more effective than argon remelting. The arrival of metal at the bath in the form of fine droplets and vertical movement of the Card 3/6

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Card 4/6

22973

S/180/61/000/003/001/012 E111/E135

Removal of oxygen in arc vacuum remelting of special steels crystallization front also contribute to mechanical removal of inclusions. It has been shown that repeated arc remelting of □ X -15 (ShKh-15) steel (0.0045% 0, 0.018 S, 0.38 Mn) reduces the inclusions greatly and that the effect is not due to increased time in the molten state (variations represented by different ingot weights) but by the remelting process itself. The demonstrated decisive role of mechanical factors as distinct from the carbon reaction in vacuum arc remelting of special steels provides a theoretical justification for applying the method irrespective of There are 2 figures, 3 tables and 8 references: carbon content. 3 Soviet and 5 English. The four most recent English language references read as follows: Ref.2: W.W. Dyrkacz, J. Metals, 1957, v. 9, December. Ref.4: E.W. Johnson, J.T. Hahm, B. Itoh. Arcs in inert atmospheres and vacuum, 1956. Ref. 5: H. Gruber. Arcs in inert atmospheres and vacuum, 1956. Ref.6: H. Gruber. J. Metals, 1958, v. 10, No.3. SUBMITTED: May 30, 1960

s/180/61/000/003/011/012 E073/E535

18.7530 1555, 1454, 1418

AUTHORS:

Vertman, A.A. and Samarin, A.M. (Moscow)

TITLE:

Viscosity of Liquid Alloys of the System Nickel-

Aluminium

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Metallurgiya i toplivo, 1961, No.3, pp.159-160

Chemical interactions in liquid solutions are apparently an indication of the strong bond in solid solutions TEXT: and permit determining the form in which an alloying component From this point of view it is of interest to investigate nickel-aluminium alloys which form the basis of numerous is present. important high temperature alloys. With the exception of a paper by V. N. Yeremenko, V. I. Inzhenko and Yu. V. Naydich (Ref. 1: Izv. AN SSSR, OTN, Metallurgiya i toplivo, 1961, No.3) the authors are not aware of any other published work on the subject. Nickelaluminium alloys were smelted in a high frequency vacuum furnace with a residual pressure of 10 mm Hg, using 99.9% purity nickel and high purity aluminium. The viscosity was determined by means of a viscosity meter, described earlier, in a pure helium atmosphere which was passed through activated carbon at the boiling Card 1/4

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22983

Viscosity of Liquid Alloys of the ... S/180/61/000/003/011/012 E073/E535

temperature of liquid nitrogen. The viscosity was calculated according to the method of Shvidkovskiy; the obtained results on the kinematic viscosity of liquid NiAl alloys in the temperature range 1600-1700°C are presented in a graph. The temperature dependence of the viscosity in this system is slight and, therefore, it can be assumed that the viscosity curve applies to the The single maximum for the NiAl temperature range 1600-1700°C. composition and the absence of any influence on the viscosity of the Ni₃Al compound which forms as a result of the pertitectic reaction is of interest. The single maximum on the viscosity curve shows that the near-order structure characteristic for the NiAl compound is maintained in the liquid state. Judging from the value of the maximum on the kinematic viscosity curve the NiAl dissociates little in the investigated temperature range. Apparently the chemical interaction in alloys corresponding to NiAl is so large that these can be considered as stable groupings. On the other hand, NigAl does not show any influence on the viscosity of the melt, which is attributed to the presence of a wide temperature range between the liquidus and the solidus, as Card 2/4

22983

Viscosity of Liquid Alloys of ... S/180/61/000/003/011/012 E073/E535

a result of which the hereditary structure of the solid phase is not conserved in the formed homogeneous liquid solution. obtained by the authors confirm the results obtained by Yeremenko in measuring the surface tension (Ref.1). An exception is their conclusion on partial dissociation of NiAl in the melt. Apparently it is correct to consider that NiAl is an extremely strong compound for which the degree of dissociation in the temperature To study the thermal range under investigation is negligible. stability of NiAl in the melt a series of tests were carried out with levitation melting followed by quenching in a copper mould. The specimens were in the form of a hollow nickel ampoule with a threaded-in lid, inside which a stoichiometric quantity of Al was placed. As a result of heating of the nickel ampoule in the magnetic field, the aluminium melts. As soon as the nickel melts there will be an intensive reaction of combination of Al with Ni which is accompanied by a sudden rise in the temperature by 300-400°C. The reaction was made easier by the intermixing of the metal in the Apparently the chemical interaction between the Ni and the Al is so strong that the NiAl forms almost instantaneously and is very stable in the liquid state up to fairly high temperatures. Card 3/4

Viscosity of Liquid Alloys of ... S/180/61/000/003/011/012 E073/E535

There are 1 figure and 2 Soviet references.

SUBMITTED: March 18, 1961

[Abstractor's Note: This is an almost complete translation]

Figure

Card 4/4

SAMARIN, A.M.; RUDNEVA, A.V.; ZALESSKAYA, S.V.

Effect of the phase composition of slags on the process of cast iron gravitation in the reduction smelting of red pulp sinters. Izv.vys. ucheb.zav.; chern.met. 4 no.6:20-26 '61. (MIRA 14:6)

1. Institut metallurgii im. A.A.Baykova. (Cast iron—Metallurgy) (Slag)

"APPROVED FOR RELEASE: 08/25/2000 CIA-RDP86-00513R001446920005-0

SAMARIN, A.M. (Moskva); MCHEDLISHVILI, V.A. (Moskva)

Properties of oxides in iron-chromium alloys. Izv. AN SSSR.
Otd. tekh. nauk. Met. i topl. no.4:50-52 Jl-Ag '61. (MIRA 14:8)

(Iron-chromium alloys-Metallography)

s/180/61/000/005/001/018 E111/E535

Averin, V.V. and Samarin, A.M. (Moscow) **AUTHORS:**

On the thermodynamics of oxygen in liquid metals and

TITLE: alloys

CANCEL PRESIDENT AND AND AND AND AND AND ADDRESS OF THE PERSON OF THE PE

Akademiya nauk SSSR. Izvestiya. Otdeleniye PERIODICAL:

tekhnicheskikh nauk. Metallurgiya i toplivo,

no.5, 1961, 3-10

The authors point out that oxygen, which is present in the vast majority of metallurgical processes, has a deleterious effect on metal properties. The authors have made previous contributions to the thermodynamics of oxygen in melts (Ref. 3: Sb. Fiziko-khimicheskiye osnovy proizvodstva stali. Izd-vo AN SSSR, 1960; Ref.5: Ibid, 1961), and in the present work they analyse conditions leading to delay in the decrease of oxygen concentration in melts and the appearance of an oxygensolubility minimum at a definite deoxidizer-concentration. Analysis of deoxidation under gas of known composition showed that the decrease in oxygen content of the melt under the action of the deoxidizer is due to two simultaneous opposed processes: a) decrease in the oxidizing potential over the melt, Card 1/9

On the thermodynamics of oxygen ... S/180/61/000/005/001/018 E111/E535

 P_0^2 compared with the value corresponding to the liquid metal P_0^2 saturated with oxygen, which leads to a decrease in oxygen saturated with oxygen, which leads to a decrease in oxygen concentration in the melt; b) increase in bond strength of the coxygen in the melt, leading to an increase in oxygen concentration oxygen in the melt compared with the liquid metal (at constant P_0 and in the melt compared with the liquid metal (at constant P_0 and P_0 are P_0 and P_0 and P_0 and P_0 and P_0 and P_0 are P_0 and P_0 and P_0 and P_0 and P_0 are P_0 and P_0 and P_0 are P_0 and P_0 and P_0 are P_0 are P_0 and P_0 are $P_$

$$\gamma_{o} = \gamma_{o}^{o} \cdot f_{o} \cdot f_{o}^{R} , \qquad (4)$$

where γ^0 is the Raoult activity coefficient for oxygen at infinite dilution in the Me-O system, f the Henry activity coefficient for oxygen at concentrations tending to zero and f the change in the activity coefficient of oxygen effected by the deoxidizer element. f represents the ratio of oxygen the deoxidizer element. f represents the ratio of oxygen concentrations in the original metal and in the melt with a definite concentration of the deoxidizer element (P being definite concentration of the deoxidizer element (P)

constant). The interaction parameter ε_0^R is given by:

On the thermodynamics of oxygen ... S/180/61/000/005/001/018 E111/E535

$$\frac{d \ln P_{0_{2}}^{1/2}}{dN_{R}} - \frac{d \ln N_{o}}{dN_{R}} = \varepsilon_{o}^{R}$$
 (11)

where N and N are the mol fractions of oxygen and deoxidizer, respectively. The authors consider next the reaction of melts with a steam-hydrogen mixture, which is informative both on the solubility and the activity of oxygen. In the general form the reaction is:

$$y_{\circ}^{H}_{2(g)} + R_{x}^{O}_{y(s,\ell)} = y_{\circ}^{H}_{2}^{O}_{(g)} + x_{\circ}^{R}_{(Me-R)}$$
 (12)

The equilibrium coefficient:

$$K = \left(\frac{P_{H_2^0}}{P_{H_2}}\right)^y \cdot a_R^x = \left(\frac{P_{H_2^0}}{P_{H_2}}\right)^y \cdot N_R^x \cdot \gamma_R^x$$
(12a)

where γ_R is the Rauolt activity coefficient for the deoxidizer Card 3/9

On the thermodynamics of oxygen ... S/180/61/000/005/001/018 E111/E535

in the system Me-R-O. Taking logarithms and differentiating

$$\frac{d \ln P_{H_2} o^{/P_{H_2}}}{dN_{R}} = -\frac{x}{y} \circ \frac{d \ln N_{R}}{dN_{R}} = -\frac{x}{y} \circ \frac{1}{N_{R}}$$
 (14)

is obtained, which holds since $K \neq f(N_R)$ and $\gamma_R \sim const$ (for low deoxidizer concentrations). Taking logarithms and differentiating for the equilibrium constant of the gaseous hydrogen + oxygen = water reaction and combining with (14) gives:

$$-\frac{x}{y} \cdot \frac{1}{N_R} - \frac{d \ln N_o}{dN_R} = \varepsilon_o^R$$
 (18)

Taking x/y values from experimental data on the change in the oxidizing potential of the gas phase in relation to deoxidizer concentration (or approximately from the value in the formula of the oxide of the deoxidizer) and knowing the value of ϵ_0 , the Card 4/9

s/180/61/000/005/001/018 On the thermodynamics of oxygen ... E111/E535

value of $N_{\overline{R}}$ at the minimum oxygen concentration can be found. The reverse calculation to find ϵ_0^R and $\epsilon_0^R = \frac{d \ln f}{d[R]}^R$ o- can also be carried out. The table shows calculated and experimental values.

	Deoxidizer concentration for Lumin				- ε R	$-\mathbf{e}_{\mathbf{o}}^{\mathbf{R}}$
Me-R melt	Calculated NR × 10°	Experimental			<u> </u>	
		R. %	R. %	•		
Fe-Cr Fe-V Fe-Si Fe-Al Ni-Fe Ni-Cr Ni-Cr Ni-V Ni-Mn Ni-Si	85.00 [2] 50.00 [10] 11.80 [2] 200.00 [2] 33.00 [13] 34.00 [14] 0.75 [15] 153.00 15.00 8.40 10.30 33.00 [4] 43.00	8.00 4.50 1.10 10.00 1.60 1.70 0.04 15.00 1.30 0.73 0.90 1.60 3.80	12.0 [9] 6.0 [11] 9.0 [12] 1.5—2.0 — 5.0—7.0 [14] 0.1—0.2 [15] 25.0 [16] 1.5—2.0 0.6—0.7 [6] 0.5—0.8 [5] 5.0 [4] 3.0—4.0		8.80 13.70 57.00 2.30 15.00 14.40 890.00 6.55 51.00 80.00 97.00 15.00 17.50	0.041 [2] 0.064 [10] 0.270 [2] 0.020 [2] 0.130 [13] 0.125 [14] 8.000 [15] 0.030 0.250 0.400 0.450 0.137 [4] 0.6086

他是我就是自己的,我们就是这个时间,我们就是这个时间的。

Card 6/9

On the thermodynamics of oxygen ... S/180/61/000/005/001/018 E111/E535

(The references given in the above table are as follows: Ref.2: Chipman, J. Atomic interaction in molten alloy steels, J. Iron and Steel Inst., 1955, June, 97; Ref.4: Sharf G., Averin, V.V., Polyakov, A.Yu., Samarin, A.M. Izv.vuzov, Chernaya metallurgiya, 1958, No.11, 29; Ref.5: Quoted earlier; Ref.6: Averin, V.V., Cherkasov, P.A., Samarin, A.M. Nauchn, dokl. po teorii zharoprochnosti. Izd-vo VPA, 1961, p.230; Ref.9:Linchevskiy, B.V., Samarin, A.M., Izv. AN SSSR, OTN, 1953, No.5; Ref.10: Turkdogan E.T., J. Iron and Steel Inst., 1954, v.178, p.278; Ref.11: Hilty D.C., Forgang W.D., Folkman R.L. Oxygen solubility and oxide phases in the Fe-Cr-O system. J.Metals, 1955, No.2; Ref.12: Averin, V.V., Samarin A.M. DAN SSSR, 1960, v.120, No.6, 1253; Ref.13: Matoba J. J. Iron and Steel Inst. Japan, 1959, 45. No.3, 229; Ref.14: Hsu Tseng-Chi, Folyakov, A.Yu., Samarin, A.M., Izv.AN SSSR, OTN, Metallurgiya i toplivo, 1961, No.2, 115; Ref.15: Kuznetsov B.M., Samarin A.M. Sb.Fiziko-khimicheskiy oxnovy proizvodstva stali. Izd-vo AN SSSR, 1961.) Next the authors consider the reaction of the water-hydrogen mixture with the deoxidizer, so as to elucidate how the oxidizing potential of the gas phase changes with changes in deoxidizing

On the thermodynamics of oxygen ... 5/180/61/000/005/001/018 E111/E535

activity. Taking the equilibrium constant for Eq. (12) in the logarithmic form and differentiating, and taking into consideration that $K \neq f(a_R)$, we obtain?

$$\frac{d \lg P_{H_2} 0^{/P_{H_2}}}{d \lg a_R} = -\frac{x}{y} . \qquad (21)$$

Finally, the following equation is obtained:

$$\frac{d \log \frac{P_{H_2} 0}{P_{H_2}}}{x \cdot \frac{d \log N_R}{d \log N_R}} + \frac{d \log \gamma_R}{d \log N_R} + 1 = 0$$
that in $\log \frac{P_{H_2} 0}{P_{H_2}} - \log N_R$ coordinates, the tangent of

This shows that in $\lg \frac{1}{P_{H_2}}$ -- lg $N_{\overline{R}}$ coordinates, the tangent of

Card 7/9

On the thermodynamics of oxygen ... S/180/61/000/005/001/018 E111/E535

the curve is determined not only by the ratio of the stoichiometric coefficients x and y but also on the nature of the change of the activity of the deoxidizer as a function of the concentration. Two particular cases are possible for which the results obtained according to Eqs.(21) and (24) are identical: 1) for small deoxidizer concentrations γ_R is practically constant and consequently, the term d lg γ_R/d lg N_R of Eq.(24) becomes zero so that the activity becomes proportional to the concentration

$$a_{R} = \gamma_{R} \circ N_{R} = \frac{1}{100} \circ \frac{M}{M_{R}} \circ \gamma_{R} \left[R\right]$$
 (25)

where M and $M_{\mbox{\scriptsize R}}$ are respectively the atomic weights of the metal and the deoxidizer and

$$\frac{d \log \frac{P_{H_20}}{P_{H_2}}}{d \log \frac{P_{H_20}}{P_{H_2}}} = \frac{d \log \frac{P_{H_20}}{P_{H_2}}}{d \log \frac{P_{H_20}}{P_{H_2}}} = \frac{d \log \frac{P_{H_20}}{P_{H_2}}}{d \log \left[R\right]} \tag{26}$$

Card 8/9

On the thermodynamics of oxygen ... S/180/61/000/005/001/018 E111/E535

In this case all equations expressing the concentration of the deoxidizer lead to equal results. 2) In the range of high deoxidizer concentrations $N_R = a_R$ and, accordingly, the derivative d lg γ_R/d lg $N_R = 0$. Except for the first two terms, Eq.(26) holds for only a limited range of concentrations even in ideal solutions, due to the fact that the atomic weights differ. There are 4 figures, 1 table and 16 references: 11 Soviet and 5 non-Soviet. The four latest English-language references read as follows: Refs.2, 11, 13 (quoted in text) and Ref.16: Wriedt, H.A. Chipman, J. Oxygen in liquid iron-nickel alloys, Trans, AIME, 1956, v.206, 1195.

SUBMITTED: March 10, 1961

Card 9/9

"APPROVED FOR RELEASE: 08/25/2000 CIA-RDP86-00513R001446920005-0

30081 \$/048/61/025/011/027/031 B117/B102

Phase equilibrium in the ...

4 hr (nes. 1-9) and for 1 hr (nos. 10-12). Specimens no. 7 were found to consist of one phase, and specimens nos. 2-6 and nos. 8-20 to consist of two phases. The bright phase in no. 2-6 seemed to be hematite, whereas the dark one appeared to be barium hexaferrite Ba0.6Fe203. The bright phase in nos. 8-20 was barium hexaferrite. The dark one could not be identified and was designated as X-phase. In almost all ferrites, the three phases showed constant hardness throughout the above-mentioned periods of time and at every sintering temperature. The saturation magnetization was examined on specimens of the quasibinary Fe203 - Ba0 system after sintering at 1200°C for 8, 16, 24, and 32 hr, and by grinding them intermittently. The saturation magnetization as a function of composition, was found to have a maximum for specimen no. 7, and dropped linearly on either side of it. This shows that two phases exist in the ranges of 0-14 3% of BaO and 14.3-50% of BaO: a magnetic (BaO:6Fe₂O₂) and a nonmagnetic phase. It is hematite in the range mentioned first, and evidently Ba0.Fe203 in the other. The Curie temperature was measured on In the range of 14 3-500 of BaO the Curie point was the same specimens Cara aff

30081 s/048/61/025/011/027/031 B117/B102

Phase equilibrium in the ...

constant, which is indicative of the heterogeneity of this range. In the range of compositions from no. 7 to 9 the Curie point is lowered, probably due to the presence of a homogeneous region. In the range up to 14.3% of BaO the Curie point was anomalously reduced for specimens nos. 2, 3, and 4, after 16-32 hr of sintering. This is probably a consequence of the change in the composition or in the structure of the ferrimagnetic phase (barium hexaferrite). In specimens nos. 2-6, which were sintered at 1200°C for 24 and 32 hr, heterogeneity was established by means of X-ray structural analysis. The specimens sintered for 24 hr consist of hematite and barium hexaferrite. On an increase of the BaO content in the mixture, the hexaferrite lines become more intense, while the hematite lines turn weaker. In specimens sintered for 32 hr it was established that with increasing BaO content the lattice constant of barium hexaferrite increases on axis a, and drops somewhat on axis c. lattice parameters are quite insignificant. Still, they exceed the experimental errors; this should not occur in the heterogeneous region of the binary equilibrium diagram. There are 4 figures, 1 table, and 3 references: 1 Soviet and 2 non-Soviet. The reference to the Englishlanguage publications reads as follows: Yasumasa Goto, Toshia Takada, J. card 3/5-/

"APPROVED FOR RELEASE: 08/25/2000 C

CIA-RDP86-00513R001446920005-0

30081 s/048/61/025/011/027/031 B117/B102

Amer. Ceram. Soc., 43, 150 (1960).

Phase equilibrium in the ...

Table: Compositions of examined specimens.

Legend: (1) no. of specimen; (2) molar ratio; (3) mole, BaO.

Card 4/84

S/020/61/139/006/014/022 B103/B101

AUTHORS:

Baratashvili, I. B., Fedotov, V. P., Samarin, A. M., Corresponding Member AS USSR, and Berezhiani, V. M.

TITLES

Solubility of nitrogen in liquid manganese

PERIODICAL: Akademiya nauk SSSR. Doklady, v. 139, no. 6, 1961, 1354-1355

TEXT: Since the data published on the solubility of nitrogen in liquid manganese are contradictory, the authors studied this problem by the method of dynamic equilibrium established between liquid manganese and nitrogen or a nitrogen - hydrogen mixture. The activity of N₂ in the metal corresponds to the partial pressure of N₂ in the gaseous phase at the instant of equilibration. The nitrogen content corresponding to the equilibrium was determined in a specimen of the solid, rapidly cooled metal. Methods and apparatus were described by A. M. Samarin, V. P. Fedotov (Tr. IV Konfer. po fiziko-khimicheskim osnovam proizvodstva stali (Proceedings of the 4th Conference on the Physicochemical Fundamentals of Steel Production)Izd. AN SSSR, 1960, p. 144). The metal Card 1/3

S/020/61/139/006/014/022 B103/B101

Solubility of nitrogen in liquid ...

was heated with an //[-60 (LG-60) h-f tube generator. Mn melt was purified with purified hydrogen (400 ml/min) for 1 hr. Subsequently, it was cooled and again molten (Test series I and II). The melt was subjected to the action of N_2 or N_2+H_2 for 120 - 180 min at a given temperature and with a given consumption of H_2 and N_2 (40 and 1100 ml/min, respectively) (series I). In the second series, the treatment was performed within 30, 60, 90, and 120 min. In the third series, Mn with a nitrogen content of 3.3 and 6.0% was treated as stated above but without previous purification in H_2 . The nitrogen content of Mn was chemically determined. It is noted that equilibrium at the same temperature is attained both by saturating the Mn melt with nitrogen and by denitrifying the nitrogen-containing Mn. Keeping the manganese in the gas current for 1 hr is sufficient for reaching equilibrium. The solubility of nitrogen decreases with increasing temperature. This function is given by $1/2 N_2(g) \rightleftharpoons N$, $K = a_N/P_{N_2}^{1/2} = f_N N / P_{N_2}^{1/2} (1)$. As a standard state, an Mn melt is taken, which is in Card 2/3

Solubility of nitrogen in liquid ... S/020/61/139/006/014/022 B103/B101

equilibrium with N_2 having a pressure of 1 atm. According to experimental data, the following relations are obtained for $P_{N_2} = 1$ atm and $f_{N} = 1$:

$$log K = log[% N] = 3010/T - 1.457; (2);$$

$$\Delta F^{\circ} = -13,780 + 6.65 T$$
 (3).

There are 2 figures and 6 references: 3 Soviet and 3 non-Soviet.

ASSOCIATION: Institut metallurgii im. A. A. Baykova Akademii nauk SSSR (Institute of Metallurgy imeni A. A. Baykov, Academy of Sciences USSR)

SUBMITTED: April 29, 1961

Card 3/3

S/020/61/140/002/022/023 B130/B110

AUTHORS:

Baratashvili, I. B., Fedotov, V. P., Samarin, A. M., and

Berezhiani, V. M., Corresponding Member AS USSR

TITLE:

Solubility of nitrogen in manganese-iron and manganese-

silicon melts

PERIODICAL:

Akademiya nauk SSSR. Doklady, v. 140, no. 2, 1961, 423-425

TEXT: The solubility of nitrogen and nitrogen-hydrogen mixtures in Mn-Fe and Mn-Si melts is calculated by the method of dynamic equilibrium between melt and gaseous phase. Apparatus and method were the same as indicated by A. M. Samarin, V. P. Fedotov (Tr. IV Konfer. po fiziko-khimicheskim osnovam proizvodstva stali, Izd. AN SSSR, 1960, p. 144). The Fe and Si content changed during melting by 2-3%. Results of determination of the solubility of nitrogen are given in Figs. 1 and 2. From the experimental data, the dependence of the coefficient of nitrogen activity in Mn-Fe and Mn-Si melts on the Fe and Si concentration in the melts is given: (a).

 $a_N^{Mn-Si(Fe)} = f_N [\%N]_{Mn-Si(Fe)}$ $a_{N}^{Mn} = f_{N} [\%N]_{Mn},$

Card 1/12

Solubility of nitrogen ...

S/020/61/140/002/022/023 B130/B110

Thus, at constant pressure and constant temperature under equilibrium conditions,

 $a_N^{Mn} = a_N^{Mn-Si(Fe)}, f_N[\%N]_{Mn} = f_N[\%N]_{Mn-Si(Fe)}$ (b)

The solubility of nitrogen in liquid Mn at $p_{N_2} = 1$ atm and T = const is taken as standard. Then, $f'_N = 1$ and $f_N = \frac{[\% N]_{Mn}}{[\% N]}$. (1). Si causes

a stronger decrease of N solubility than Fe. Also an increase in the temperature of the melt reduces the N sclubility (Fig. 4). log K and ΔF^O were calculated from the experimental data given in Fig. 4. Calculation results are given in Table 1. There are 4 figures, 1 table, and 3 Soviet references.

ASSOCIATION:

Institut Metallurgii im. A. A. Baykova Akademii nauk SSSR (Institute of Metallurgy imeni A. A. Baykov of the Academy

of Sciences USSR)

SUBMITTED:

May 11, 1961

Card 2/6

"APPROVED FOR RELEASE: 08/25/2000 CIA-RDP86-00513R001446920005-0

SAMARIN, A.M., otv. red.; RYKALIN, N.N., otv. red.; ZOLOTOV, P.F., red. 12d-va; SUSHKOVA, L.A., tekhn. red.

[Steel made of Kerch Peninsula ores] Stal' iz kerchenskikh rud. Moskva, Izd-vo Akad. nauk SSSR, 1962. 90 p. (MIRA 15:6)

1. Akademiya nauk SSSR. Institut metallurgii. 2. Chlenkorrespondent Akademii nauk SSSR (for Samarin, Rykalin). (Steel-Metallurgy) (Kerch Peninsula-Iron ores)

GAYUI, Rene Zhyust [Hauy, Rene-Just]; SHAFRANOVSKIY, I.I., prof.;
ZABOTKINA, O.S.[translator]; STRATANOVSKIY, G.A.[translator];
SHUENIKOV, A.V., akademik, red.; BOKIY, G.B., red.;
PETROVSKIY, I.G., akademik, red.; ANDREYEV, N.N., akademik, red.;
KAZANSKIY, B.A., akademik, red.; YUDIN, P.F., akademik, red.;
DELONE, B.N., red.; SAMARIN, A.M., red.; ZUBOV, V.P., prof., red;
LEBEDEV, D.M., prof., red.; FIGUROVSKIY, N.A., prof., red.;
KUZNETSOV, I.V., kand. filos. nauk, red.; OZNOBISHIN, D.V., kand.
istor. nauk, red.; SUSHKOVA, T.I., red. izd-va; SHIRNOVA, A.V.,
tekhn. red.

[Structure of crystals; selected works] Struktura kristallov; izbrannye trudy. Sostavlenie, statia i primechaniia I.I. Shafranovskogo. Redaktsiia A.V.Shubnikova i G.B.Bokiia. Moskva, Izd-vo Akad. nauk SSSR, 1962. 175 p. Translated from the French.

(MIRA 15:3)
1. Chlen-korrespondent Akademii nauk SSSR (for Bokiy, Delone, Samarin).

(Crystallography)

SAMARIN, A.M., red.; PTITSYNA, V.I., red. izd-va; DOBUZHINSKAYA, L.V., tekhn. red.

[Vacuum metallurgy]Vakuumnaia metallurgiia. Moskva, Metallurgizdat, 1962. 515 p. (MIRA 15:12)

1. Chlen-korrespondent Akademii nauk SSSR (for Samarin) (Vacuum metallurgy)

SAMARIN, A.M. Principal directions in the expansion of the technology of ferrous metal production. Izv. AN SSSR. Otd. tekh. nauk. Met. i topl. no.2:3-8 Mr-Ap '62. (Iron--Metallurgy) (Steel--Metallurgy) (Iron--Metallurgy)

BURTSEV, V.T. (Moskva); KARASEV, R.A. (Moskva); SAMARIN, A.M. (Moskva)

Sulfur vapor pressure in contact with iron - sulfur melts. Izv.
AN SSSR. Otd. tekh. nauk. Met. i topl. no.2:42-48 Mr-Ap '62.

(MIRA 15:4)

(Vapor pressure--Measurement) (Desulfuration)

GARNYK, G.A.; SAMARIN, A.M.

Effect of certain elements on the properties of electrical engineering steel. Elektrichestvo no.2:71-74 F '62. (MIRA 15:2)

1. Institut metallurgii im. Baykova. (Steel)

GOAN' AN'-MIN' (Moskva); MCHEDLISHVILI, V.A. (Moskva); SAMARIN, A.M. (Moskva)

Process of steel deoxidation by complex alloys of silicon, manganese, and aluminum. Izv.AN SSSR. Otd.tekh.nauk. Met.i topl. no.4:31-39 Jl-Ag '62. (MIRA 15:8) (MIRA 15:8)

(Steel-Metallurgy)

S/148/62/000/005/001/009 E071/E135

Vertman, A.A., Mchedlishvili, V.A., and Samarin,

The influence of deoxidation on the viscosity of AUTHORS:

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Chernaya

metallurgiya, no.5, 1962, 34-36

The effect of deoxidation of steel by a deoxidising element depends to a considerable extent on the velocity of flotation of products of the deoxidising reaction. Since there are no direct methods of measuring the velocity of flotation of are no direct methods of measuring the vertex attempted non-metallic inclusions from a liquid metal, the authors attempted to evaluate this velocity from results of changes in the kinematic viscosity of liquid iron during its deoxidation with silicon and aluminium. The viscosity was determined from the torsional vibrations of a cylinder filled with the liquid investigated.

The experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with additions of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiments were carried out at 1600 °C with addition of the experiment 0.1 and 1.0% Si and 0.5 and 1.0% Al to armco iron, in an atmosphere of purified helium in a furnace with graphite heating elements, so as to exclude the possibility of reoxidation. Card 1/2

S/148/62/000/005/001/009 The influence of deoxidation on ... E071/E135

In all the experiments addition of the deoxidant resulted first in an increase of the viscosity, due to heterogenisation of the liquid metal caused by the formation of deoxidation products; this was followed by a steady decrease in viscosity which approached its initial value for pure iron. The time taken to reach the initial viscosity after the addition of a deoxidant can serve as a measure of the velocity of flotation of deoxidation products. The duration of flotation of products formed on the addition of 0.5 and 1% Al was 2-3 minutes. On adding 0.1% Al the velocity of flotation decreased considerably: the initial viscosity was not attained after a considerable time (25 minutes). Addition of 1% Si had a similar effect; on adding 0.1% Si the velocity of flotation is considerable, after about five minutes the deoxidation products were removed. This confirms that the deoxidation with large quantities of aluminium is more effective than deoxidation with silicon or small additions of aluminium. There are 2 figures.

ASSOCIATION: Institut metallurgii AN SSSR

Card 2/2 (Institute of Metallurgy, AS USSR)

October 4, 1961 SUBMITTED:

1

S/659/62/009/000/028/030 I003/I203

AUTHORS

Averin, V. V., Cherkasov, O. A., and Samarin, A. M.

TITLE:

Deoxidation of molten nickel

SOURCE

Akademiya nauk SSSR. Institut metallurgii. Issledovaniya po zharoprochnym splavam.

v. 9. 1962. Materialy Nauchnoy sessii po zharoprochnym splavam (1961 g.),205-218

TEXT: Nickel-base heat-resisting alloys are widely used in the jet plane, and rocket industry. The influence of deoxidizing elements such as iron, cobalt, chromium, manganese, vanadium, titanium, silicon, carbon, and aluminum on both the solubility and on the activity of oxygen in molten nickel was investigated. It was also shown that the activity of these elements is actually lower in nickel than in iron, which is in good agreement with the values for the heat of formation of intermetallic compounds of the type Ni_xR, and Fe_xR, A comparison was made between the influence of the above deoxidizing agent on the activity of oxygen in molten nickel and in molten iron. A relationship between the decrease in activity of oxygen and its minimum solubility was found. In the discussion, A. V. Emyashev pointed out that the total oxygen content in nickel does not determine its properties, as about 80% of the oxygen is bound in the form of oxides, and it is the non-metallic inclusions which must be taken into account. There are 5 figures and 3 tables

Card 1/1

Desulfuration of liquid iron in vacuum. Izv. vys. ucheb. zav.; chern. met. 5 no.5:86-93 '62. (MIRA 15:6)

1. Institut metallurgii im. Baykova.
(Iron-metallurgy) (Desulfuration)

YASKEVICH, A.A.; SAMARIN, A.M.

Effect of nitrogen and boron on the properties of austenitic stainless steel. Izv. vys. ucheb. zav.; chern. met. 5 no.7: 97-102 '62. (MIRA 15:8)

1. Moskovskiy institut stali i splavov.
(Steel, Stainless-Metallurgy)

10

s/032/62/028/010/003/009 B117/B186

AUTHORS:

Burtsev, V. T., and Samarin, A. M.

TITLE:

Investigation of saturated vapor pressures of liquid metals and their impurities by the carrier gas technique

Zavodskaya laboratoriya, v. 28, no. 10, 1962, 1199-1203

TEXT: The accuracy of the carrier gas technique for determining the pressures of saturated metal vapors above 10-2mm Hg is checked. It is PERIODICAL: shown that errors are caused by variations in the velocity of the carrier gas, vapor condensation, holding time, and extrapolation of the results. Determination of saturated silver vapor at 1150 and 1250°C using argon shows that the maximum total error of this technique is ~7 %. Comparison between experimental results and published data (J. Elliott, M. Gleiser, Thermochemistry for Steelmaking, Addison-Wesley Publishing Co., London

(1961)) shows a divergence of 2 to 3 %. Data on iron vapor determined at 1580-1680°C differed from reference values by 2.5-3%. Determination of the partial pressure of saturated sulfur vapor above iron-sulfur melts (sulfur content, 0.067-0.57 %) indicates that the sulfur escaping from

Card 1/2

OVED FOR RELEASE: 08/25/2000

s/030/62/000/002/002/008 B105/B110

AUTHOR:

Samarin, A. M., Corresponding Member AS USSR

Research into the physical and chemical fundamentals of

TITLE:

metallurgical techniques

PERIODICAL:

Akademiya nauk SSSR. Vestnik, no. 2, 1962, 35 - 37

TEXT: The author gives a brief report of new scientific studies that serve the perfection of techniques of obtaining metals from natural raw materials, of metal and alloy refining, of increasing the quality of the products and of improving the commercial and economic indices. In this connection oxygen and natural gas are mentioned as new means. The author mentions the production of ultra pure metals and alloys and the improvement of the steel and alloy properties, the production of super-strength steels and alloys with special properties for machine constructions and apparatus operating at high and superhigh temperatures and pressures or at high speeds. He discusses the necessity of processing combines and agglomerating plants in order to increase the furnace capacity. Special emphasis is laid upon the industrial use of low and superhigh pressures Card 1/2

Research into the physical ...

S/030/62/000/002/002/008 B105/B110

and of atmosphere with low oxidation potential: vacuum treatment of liquid steel, casting of steel and alloys in the vacuum or in an inert-gas atmosphere melting and casting of steel and alloys in vacuum furnaces; production of metals and iron alloys by reducing the oxides and other metal compounds in the vacuum, decarbonization of metals and alloys in the vacuum, decomposition of various compounds and evaporation of impurities in the vacuum. The most important task is considered to be the determination of the thermodynamic functions of metallurgical reactions and the study of the kinetics of these reactions, the determination of the effect of surface energy in steel melting, the prevention of interaction between metal and vacuum furnace lining. To perfect the technique of continuous casting and rolling, it is necessary to study the structures of metallic melts, to determine methods of changing them, and to introduce optimum methods of ordering the crystalline structure of steel and alloys.

Card 2/2

s/020/62/143/001/027/030 B101/B147

AUTHORS:

Mchedlishvili, V. A., Samarin, A. M., Corresponding Member

AS USSR

TITLE:

Oxide inclusions in iron - vanadium alloys

PERIODICAL: Akademiya nauk SSSR. Doklady, v. 143, no. 1, 1962,

159 - 161

TEXT: The authors studied deoxidation products forming in liquid electrolytic iron on the addition of vanadium of 0.064, 0.13, 0.18, 0.25, and 0.85%. V was added in the form of ferrovanadium. Samples taken between 1560 and 1580° C were electrolytically dissolved, and the anodic deposit was studied microscopically and radiographically. Results: (1) On increasing the V content to 0.18%, the shape of oxide inclusions changes from irregular and globular to clearly rhombic and octahedral forms. At 0.25% V, only rhombic and rectangular forms were observed. (2) The particles are highly magneticat <0.25% V, and nonmagnetic at >0.25% V. The radiographic lines of these two groups differ. (3) Calculations of

Card 1/2

CIA-RDP86-00513R001446920005-0" APPROVED FOR RELEASE: 08/25/2000

S/020/62/143/001/027/030 B101/B147

Oxide inclusions ...

interplanar spacings showed the structure of inclusions with <0.25% V to be that of vanadium spinel, FeV₂O₄, with isomorphic substitution of V: Fe²⁺(Fe³⁺, V³⁺)₂O₄. At a very low V content, the structure of the inclusions is similar to that of Fe₃O₄ which explains their magnetic properties. At >0.25% V, the structure of inclusions is almost identical with that of V₂O₃. There are 1 figure, 1 table, and 2 references: 1 Soviet and 1 non-Soviet. The reference to the English-language publication reads as follows: Cumulative Alphabetical and Grouped Numerical Index of X-Ray Diffraction, Philadelphia, 1953.

SUBMITTED: November 18, 1961

Card 2/2

VOLKOV, S.Ye. (Moskva); SAMARIN, A.M. (Moskva)

Effect of the silicon reduction of steel on the process of its desulfuration. Izv. AN SSSR. Otd. tekh. nauk. Met. i topl. no.3: 20-26 My-Je 162. (MIRA 15:6)

(Steel-Metallurgy) (Desulfuration)

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5/180/62/000/006/001/022
                                                                                                                                                                                                                                                                                     E193/E383
                                                                             Vertman, A.A., Samarin, A.M. and Filippov, Ye.S.
                                                                                   Viscosity and electrical conductivity of liquid
                                                                                                               Akademiya nauk SSSR. Izvestiya. Otdeleniye
                                                                              (Moscow)
                                                                                          tekhnicheskikh nauk. Metallurgiya i toplivo,
AUTHORS:
                                                                                      nickel-carbon alloys
                                                                                                In continuation of an earlier work (Izv. AN SSSR, OTN.
                 In continuation of an earlier work (Izv. AN SSSR, OT the authors have 1960, no. 6, 162-167) the authors have determined the concentration-dependence of viscosity and electermined the concentration dependence of viscos
     TITLE:
                      metallurglya 1 toplivo, 1900, no. 0, 102-107) the authors have determined the concentration-dependence of viscosity and electrical conductivity of liquid nickel-carbon alloys in the 0-2.
                       determined the concentration-dependence of viscosity and elec- 3% in the 0-2.3% trical conductivity of liquid nickel-carbon alloys where the carbon range. The results are reproduced in Fig. 4.
           PERIODICAL:
                         trical conductivity of liquid nickel-carbon alloys in the 0-2.3 in the 0-2.3 in the 0-2.3 in the other than the carbon range. The results are reproduced in Fig. (O. Worm viscosity (), centistokes) and electrical resistivity (O. Worm viscosity (), centistokes)
                           carbon range. The results are reproduced in Fig. 4, where the plotted resistivity (C, plotted) are reproduced in Fig. 4, where the plotted resistivity (C, plotted) are reproduced in Fig. 4, where the plotted resistivity (C, plotted) are reproduced in Fig. 4, where the plotted 
                                of the alloys at temperatures indicated by each curve are it had since it had since it had since it had some content (C, wt.%) of the alloy. Stroyenties against the carbon content (C, wt.%) vertman and properties of shown earlier (V.M. Glazov, ium. Structure and properties (Symposium. (Symposium. 124-137) that the visoroystv zhidkikh metallov (Symposium. 1960. 124-137) that of liquid metals), Izd-vo AN SSSR. 1960.
                                      svoystv zhidkikh metallov (Symposium. Structure and properties that the visof liquid metals), Izd-vo AN SSSR, 1960, 124-137) that the of liquid metals), feetestiferous systems passed through a cosit //4 Card //4
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S/180/62/000/006/001/022 E193/E383

Viscosity and

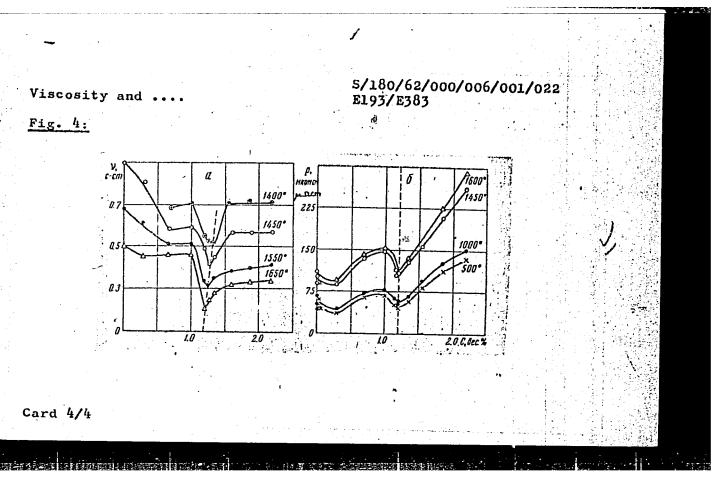
minimum at the eutectic composition (i.e. in the alloy in which the relatively weaker forces binding dissimilar atoms predominated) the curves reproduced in Fig. 4 indicated that the Ni-C eutectic was formed at 1.35% against the published value of 2.0-2.5% C. The constitution diagram of the Ni-C system was therefore reinvestigated by thermal and metallographic analysis; the results showed that the eutectic was, in fact, formed at approximately 1.3-1.4% C. It was concluded, consequently, that the minima on the viscosity and electrical-resistivity isotherms were associated with the fact that the short-range order, inherent in solid eutectic alloys was retained on melting; increasing the concentration of either Ni or C in the alloy brought about an increase in the proportion of the relatively stronger forces between similar atoms which, in turn, increased the viscosity of the alloy. The existence of viscosity hysteresis was also established. This effect was attributed to the existence of microscopic arrays of C atoms in the alloy; these dissolved partially on melting, as a result of which their size during subsequent cooling was smaller than during heating, this difference being reflected in the viscosity of the The presence of a sharp minimum in the concentrationalloy.

Viscosity and

5/180/62/000/006/001/022 E193/E383

dependence of the activation energy for the viscous flow of Ni-C alloys was also attributed to the effect of microscopic arrays of C atoms. The concentration-dependence of the $\rho_{\rm TB}$ ratio (where $\rho_{\rm TB}$ and $\rho_{\rm TB}$ denote, respectively, resistivity of the alloy in the liquid and solid states at the eutectic temperature) was also determined. The value of One of the practically constant in the hypo-eutectic alloys, increased sharply in the hypereutectic range. This effect was attributed to partial dissolution of the carbon micro-arrays on melting. The general conclusion was that the formation of carbon micro-arrays was a property common to all three systems of the Ni-C system which represent a limiting case of microheterogeneous eutectic alloys with properties. approaching those of a colloidal solution. There are 7 figures. SUBMITTED: May 8, 1962

Card 3/4



"APPROVED FOR RELEASE: 08/25/2000 CIA-RDP86-00513R001446920005-0

VERTMAN, A.A.; SAMARIN, A.M.

Structure and properties of liquid metals. Trudy Instanct.
no.10:108-134 *62. (MIRA 15:8)

(Liquid metals—Testing)

VERTMAN, A.A.; SAMARIN, A.M.

Physicochemical properties of liquid alloys of iron, nickel, and cobalt. Trudy Inst.met. no.10:135-151 '62. (MIRA 15:8) (Liquid metals—Testing) (Alloys—Testing)

"APPROVED FOR RELEASE: 08/25/2000 CIA-RDP86-00513R001446920005-0

Separation of liquid eutectics by centrifugation. Trudy Inst.
met. no.10:152-154 '62. (MIRA 15:8)

(Eutectics) (Centrifugation)

s/509/62/000/010/001/005 1003/1242

AUTHORS:

Pupynin, V.P., Hsu Tseng-chi, Polyakov, A. Yu,

and Samarin, A.M.

Investigation of the activity of the components in molten binary alloys of the nickel-carbon system

SOURCE:

TITLE:

Akademiya nauk SSSR. Institut Metallurgii. Trudy. no. 10. Moscow, 1962, 155-161. Metallurgiya, metallovedeniye, fiziko-khimicheskiye metody

issledovaniya

The investigation of the thermodynamic properties of molten nickel alloys is not only of theoretical interest: it serves to determine the optimum composition and the best process for the

Card 1/2

CIA-RDP86-00513R001446920005-0" APPROVED FOR RELEASE: 08/25/2000

s/509/62/000/010/005/005 1003/1203

AUTHORS:

Yang Nan-tsu, Makunin, M.S., Polyakov, A.Yu.,

and Samarin, A.M.

TITLE:

Investigation of the vacuum preparation of ferrova-

nadium and ferrotungsten

SOURCE:

Akademiya nauk SSSR. Institut metallurgii. Trudy,

no. 10. Moscow, 1962, 246-251. Metallurgiya, metallovedeniye, fiziko-khimicheskiye metody

issledovaniya

TEXT: The reduction of vanadium pentoxide in vacuum is less expensive than the present USSR process of reduction by ferrosilicon and aluminum in an electric furnace. The kinetics

Card 1/2

S/509/62/000/010/005/005 I003/I203

Investigation of the....

of the process of reduction of mixtures of vanadium and iron oxides by carbon was studied at pressures from 10-3 to 200 mm Hg and at temperatures of 600 to 1300°C. The process is very economical and yields purer products than envisaged by Soviet FOCT (GOST) standards. Briquettes of ferrotungsten obtained in an analogous process at a temperature of 1100°C and at a pressure of 0.1 mm Hg ing and sintering at 1350°-1400° in vacuum is necessary. There are 4 figures and 2 tables.

Card 2/2

ACRIKOLA, Georgiy [Agricola, Georg]; GAL'MINAS, V.A.[translator];

DROBINSKIY, A.I.[translator]; SHUKHARDIN, S.V., red.;

PETROVSKIY, I.G., akaderik, red.; ANDREYEV, N.N., akademik, red.; KAZANSKIY, B.A., akademik, red.; YUDIN, P.F., ckademik, red.; DELONE, B.N., red.; SAMARIN, A.M., red.; ZUBOV, V.P., prof., red.; LEBEDEV, D.M., prof., red.; FIGUROVSKIY, N.A., prof., red.; KUZNETSOV, I.V., doktor filos. nauk, red.;

BORODINA, R.M., red. izd-va; YEPIFANOVA, L.V., tekhn. red.;

DOROKHINA, I.N., tekhn. red.

[Mining and metallurgy; in twelve books]0 gornom dele i metallurgii; v dvenadtsati knigakh. Red. S.V.Shukhardina, perevod i primechaniia V.A.Gallminasa i A.I.Drobinskogo. Moskva, Izd-vo Akad. nauk SSSR, 1962. 597 p. (MIRA 15:8)

1. Chlen-korrespondent Akademii nauk SSSR (for Delone, Samarin).

(Mines and mineral resources)

(Metalwork)

KASIN, V., SAMARIN, A.M.

"Die entschwefelung von flussigem nickel im vakuum."

Report submitted to the 11th Congress on Mining and Metallurgy, Freiberg, GBR 13-16 June 1962

PHASE I BOOK EXPLOITATION

sov/6270

- Samarin, A. M., ed., Corresponding Member, Academy of Sciences USSR.
- Vakuumnaya metallurgiya (Vacuum Metallurgy). Moscow, Metallurgizdat, 1962. 515 p. Errata slip inserted. 3200 copies printed.
- Ed. of Publishing House: V. I. Ptitsyna; Tech. Ed.: L. V. Dobuzhin-skaya.
- PURPOSE: This book is intended for engineering personnel of metallurgical and machine-building plants, scientific research workers and teachers, and aspirants and students at schools of higher technical education.
- COVERACE: Thermoydnamic fundamentals of vacuum application in various metallurgical processes and problems of melting in vacuum induction and arc furnaces are discussed. Procedures of casting large ingots and vacuum degassing of steel in ladles are described, along with designs of metallurgical vacuum equipment. Problems connected with the use of mechanical and steam-ejector vacuum pumps, and with the

Card 1/75

sov/6270 Vacuum Metallurgy designing, calculation, and operation of vacuum systems, are reviewed in detail, along with vacuum-measuring techniques. No personalities are mentioned. Each article is accompanied by references, mostly Soviet. TABLE OF CONTENTS: 5 Foreword Polyakov, A. Yu. Thermodynamic Fundamentals of Vacuum 7 Application in the Processes of Making Steels and Alloys General laws Reactions in reduction of metal oxides with carbon 2. Deoxidation of steel 3. Degassing of metal Distillation of alloy components in vacuum-melting 5. processes Interaction of molten metal and refractory lining Card 2/75

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Vacuum Metallurgy	SOV/ 6270
Novik, L. M. Vacuum Degassing of Molten Metal (Ladle and Stream Degassing)	
1. Design of vacuum unit	76
4. Vacuum treatment of allegers	87
or rackwall treatment of and malk a se	92
rail steel, and structural Bessemer steel	100
4. Vacuum treatment of ferroalloys 5. Casting of steel and alloys in vacuum or in	102 129
a protective atmosphere	469
• New LSoviet design of large	131
melting vacuum arc furnace 7. Technical and occurred	130
7. Technical and economic effectiveness of applying vacuum processes	139
General conclusions	145
Linchevskiv P v ca	146
Linchevskiy, B. V. Steel and Alloy Melting in Vacuum	
1. Vacuum industion summa	150
2. Technology of melting stool	151
vacuum induction furnaces	167
ard 3/75	